



Energy for  
generations



# Update on RoCoF

Marios Zarifakis, ESB G&WM

## 1. Analysis of Eirgrid's KEMA Study

1. Stability – **Mechanical Impacts**
2. Limitations in the under excited area – **Operational Issues**
3. Time window in definition of Rocof. 500ms vs. 100ms sec duration of a RoCoF Event – **Unknown Requirement → Compliance Impossible**

## 2. Analysis of Study currently being undertaken by DNV GL (former KEMA) for ESB GWM

1. Ability to operate at Minimum Load – **Potentially unavailable at night i.e. when most required**

## 3. Next Steps

Generation Units Result Summary					1 Hz total frequency drop			
Generator Set	Unit Size	Inertia Constant H	Xd	Terminal Voltage	Stable	during	RoCoF	
[name]	[MW]	[Sec.]	[p.u.]	[kV]	[@ 0.5 Hz/s]	[@ 1.0 Hz/s]	[@ 1.5 Hz/s]	[@ 2.0Hz/s]
CCGT Single-shaft	400	5.5	1.9	20	Y	Y*	Y*	N
CCGT Dual-Shaft	260	6	2.3	17	Y	N	N	N
CCGT Dual-Shaft	140	9	2.1	17	Y	N	N	N
Steam Thermal (Reheat)	300	5	1.7	17	Y	Y*	Y*	N**
Steam Thermal (Once Through)	250	4.5	2.3	20	Y*	Y*	N	N
Steam Thermal (Fluidized bed peat)	150	8	2.2	11	Y*	N	N	N
OCGT	50	1.5	2.9	11	Y*	Y*	Y*	Y*
Salient-pole Hydro	30	2.7	1.4	11	Y	Y	Y	Y

The tables give a general overview of the findings where:

Y is used to indicate stable operation

Y\* is used where a pole slip is only observed for a 0.93 leading power factor operation mode;

N is used when a pole slip is also observed for power factors of 1 unity or/and 0.85 lag;

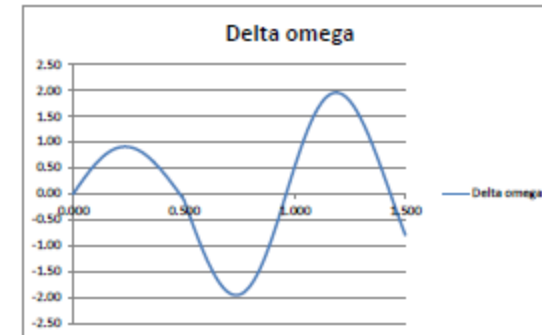
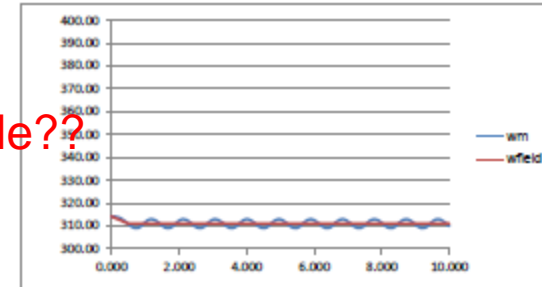
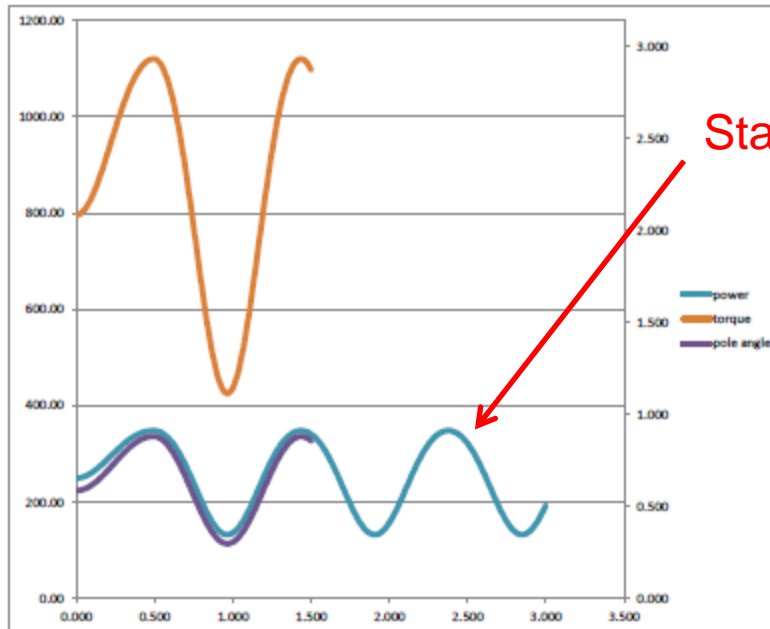
N\*\* is used when no pole slip is observed for power factors of 1 unity or/and 0.85 lag but negative power generation is detected.

# Stable: Y; Interpretation of Stability

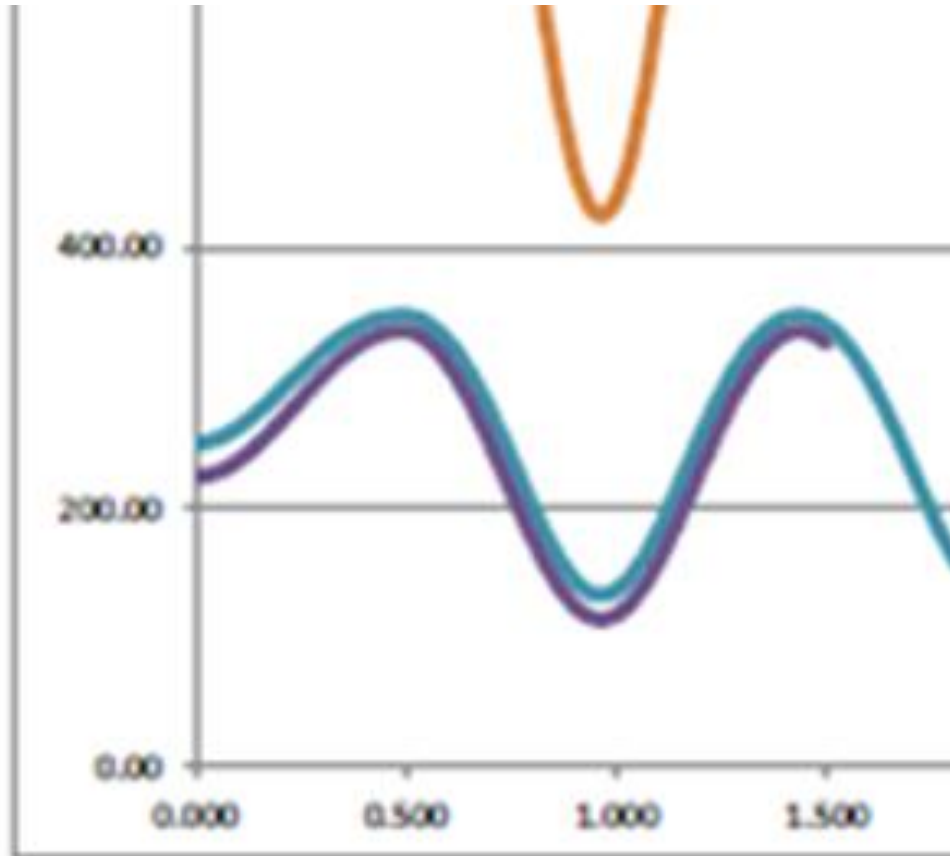
Calculation ID: E

Torque Calculation Synchronous Generator

Quantity/ Dimension	Value	SI Unit	Quantity/ Dimension	Value	SI Unit	ID	cosφ	load	RoCoF	Stable	MaxTorque	Limf
[Name/ Symbol]	[Number]	[Symbol]	[Name/ Symbol]	[Number]	[Symbol]		[-]	[%]	[Hz/s]		[%]	[Hz/s]
Rated power	250	[MW]	Reference reactance	1.360	[Ω]	E	0.85	lag	100	-1	y	141
Rated power factor	0.85		Synchronous reactance	3.128	[Ω]		φ		$\omega_{lim,stat}$			
Rated voltage	20000	[V]	$\omega_n$	314.2	[rad/s]		31.78833	*	0.59			
Synchronous reactance	2.3	[p.u.]	$\delta$	0.59	[rad]							
$f_s$	50	[Hz]	$P_{max}$	250.0	[MW]							
p (pole pair number)	1		Cpower	451.9								
H (stored energy constant)	4.5	[s]	$T_{max}$	796	[kNm]							
Rated power	294	[MVA]	J	26820	[kgm <sup>2</sup> ]							
Rated current	8490	[A]	Max. torque (500 ms)	141	[%]							
Rated torque	796	[kNm]	Max. torque (1 s)	141	[%]							



# Power Oscillations



In this example, the power, even considered stable oscillates within parts of seconds 100MW

- The term stable is used in relation to Rotor Angle Stability, i.e. Rotor does not pole slip.
- It does not mean that the generator is able to operate with such power and torque oscillations
- Further Studies are required to determine if Turbine Controller would be stable (frequency response logics)
- No review of mechanical stresses undertaken
- No review of AVR and PSS undertaken (PSS: right model?)

# Operation at 0.93 leading

Generation Units Result Summary					1 Hz total frequency drop			
Generator Set	Unit Size	Inertia Constant H	Xd	Terminal Voltage	Stable	during	RoCoF	
[name]	[MW]	[Sec.]	[p.u.]	[kV]	[@ 0.5 Hz/s]	[@ 1.0 Hz/s]	[@ 1.5 Hz/s]	[@ 2.0Hz/s]
CCGT Single-shaft	400	5.5	1.9	20	Y	Y*	Y*	N
CCGT Dual-Shaft	260	6	2.3	17	Y	N	N	N
CCGT Dual-Shaft	140	9	2.1	17	Y	N	N	N
Steam Thermal (Reheat)	300	5	1.7	17	Y	Y*	Y*	N**
Steam Thermal (Once Through)	250	4.5	2.3	20	Y*	Y*	N	N
Steam Thermal (Fluidized bed peat)	150	8	2.2	11	Y*	N	N	N
OCGT	50	1.5	2.9	11	Y*	Y*	Y*	Y*
Salient-pole Hydro	30	2.7	1.4	11	Y	Y	Y	Y

The tables give a general overview of the findings where:

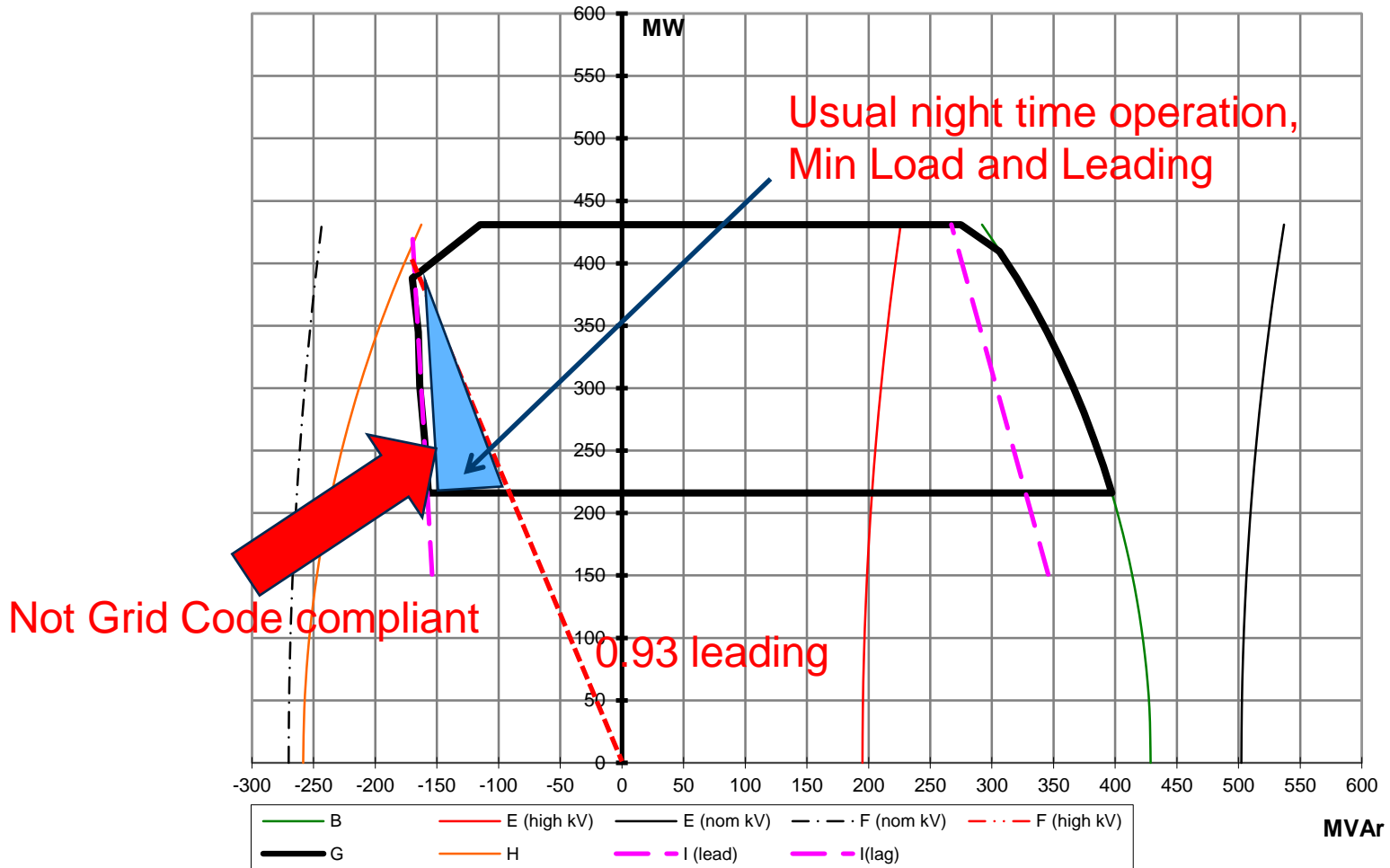
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N is used when a pole slip is also observed for power factors of 1 unity or/and 0.85 lag;

N\*\* is used when no pole slip is observed for power factors of 1 unity or/and 0.85 lag but negative power generation is detected.

# 0.93 leading, example single shaft CCGT



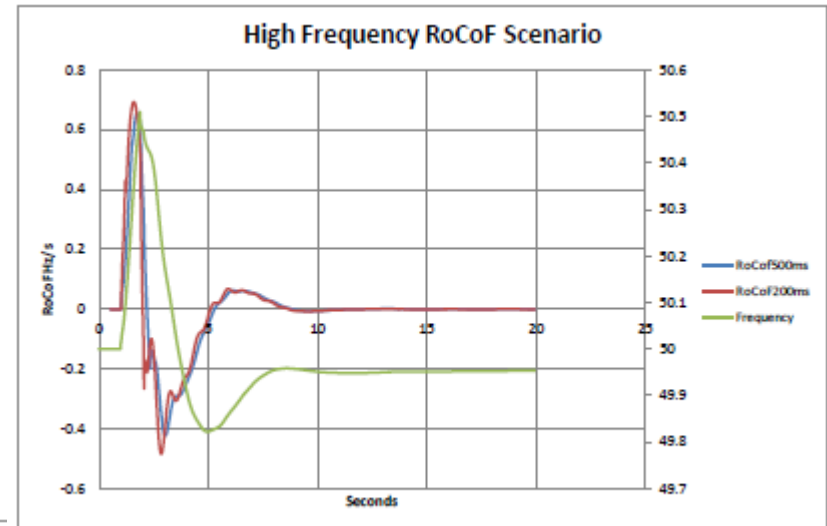
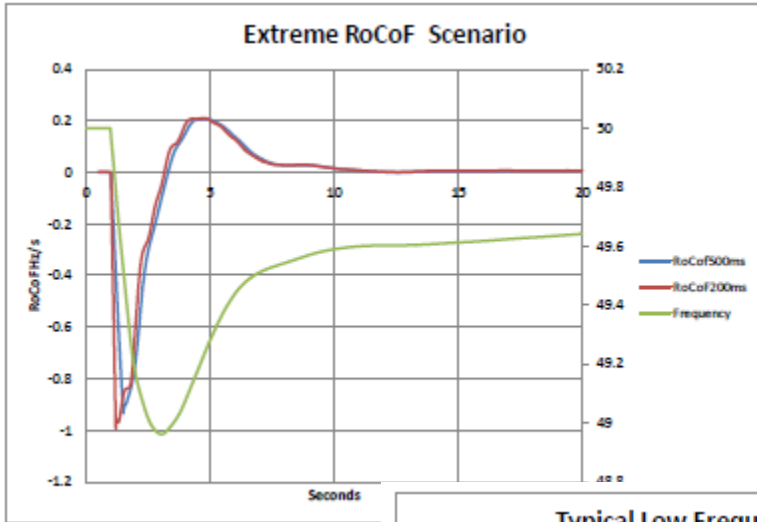


## 0.93 Leading

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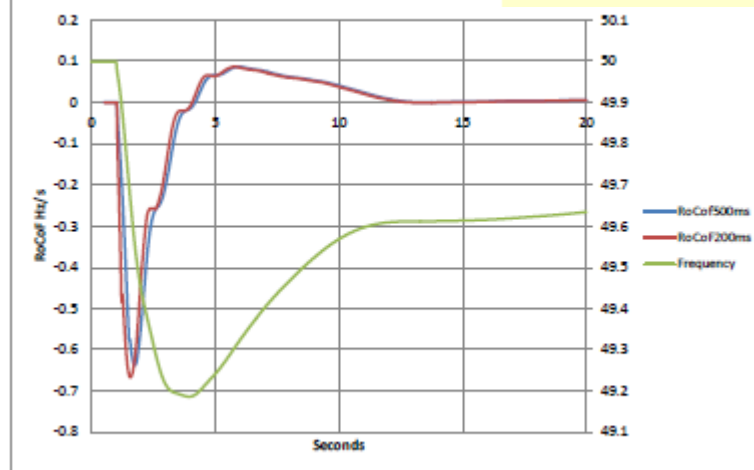
- Operation below 0.93 leading could be restricted especially at night time which means non-compliance to the grid code
- Further Studies are required to determine exact line of rotor instability during RoCoF events.

# 500ms window vs 200ms window (Eirgrid)



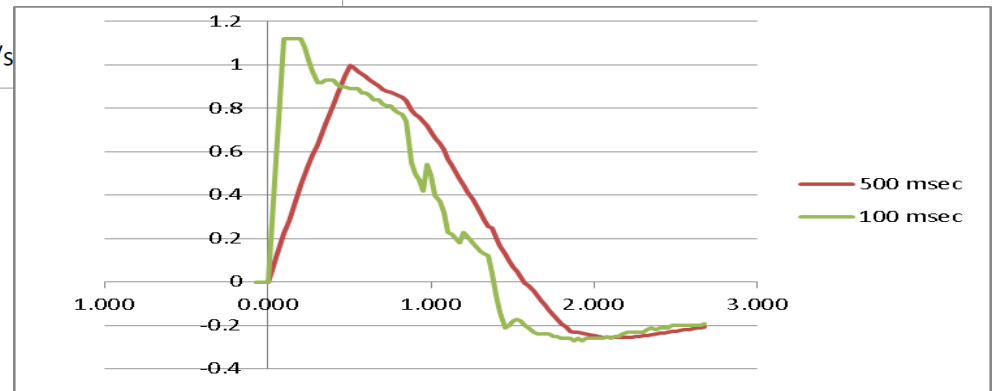
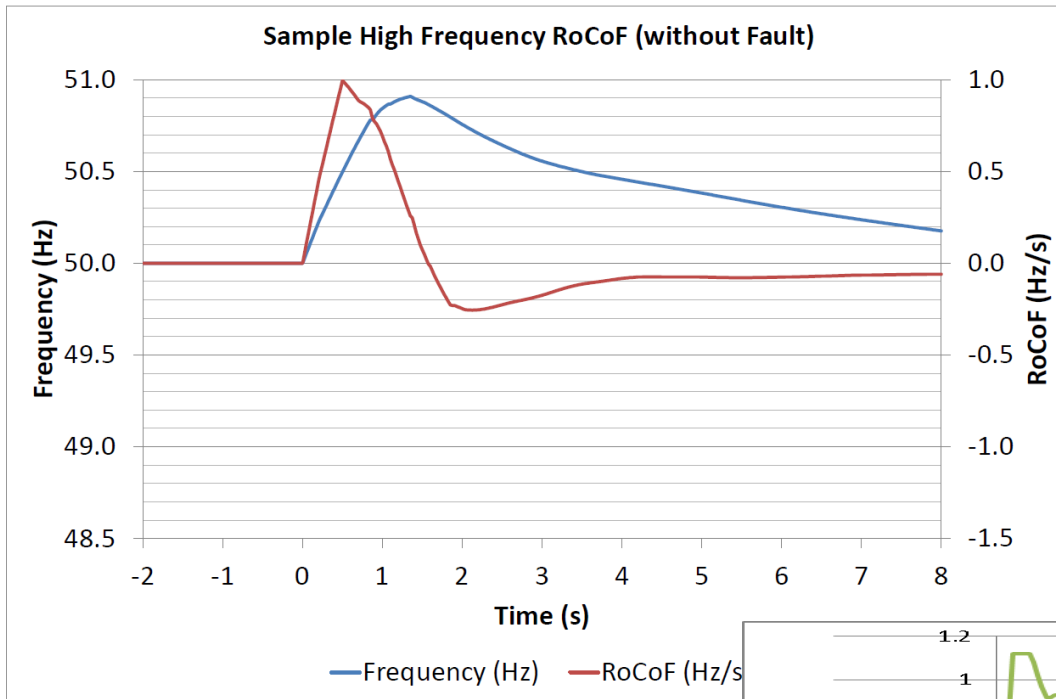
Loss of Largest Infeed / Extreme Scenario

Typical Low Frequency RoCoF Loss of Largest Outfeed / Typical Scenario

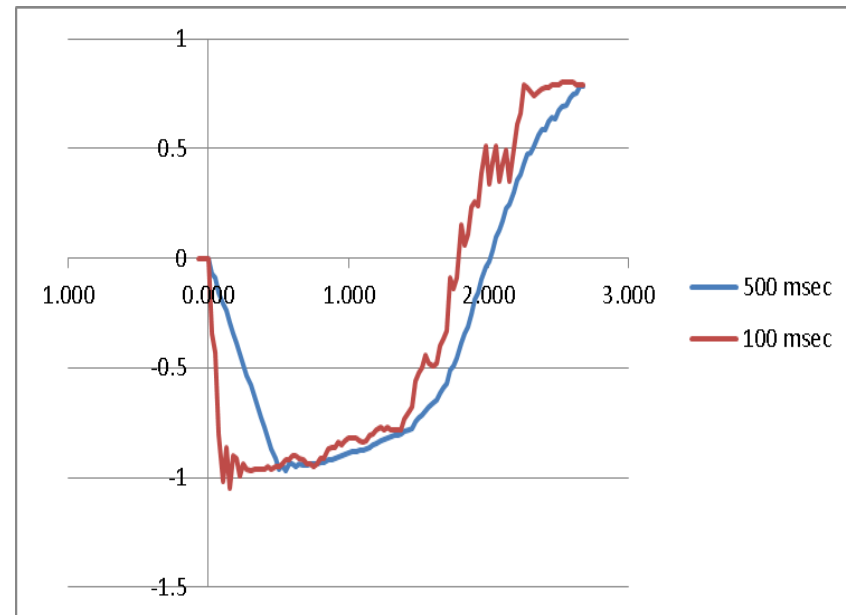
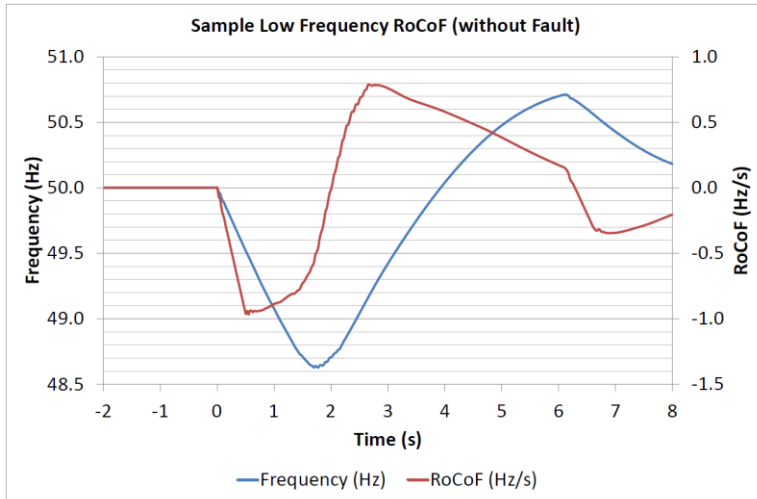


Loss of Largest Infeed / Typical Scenario

# 500ms window vs 100ms window



Duration of high RoCoF  
Is longer when time window  
Is decreased.



**Duration of high RoCoF  
Is longer when time window  
Is decreased**

# Duration of fault and it's impact

Generation Units Result Summary					500 ms v 1 Hz total frequency drop					
Generator Set	Unit Size	Inertia Constant H	Xd	Terminal Voltage	Stable during	Stable during	Stable during	Stable during	RoCoF	RoCoF
[name]	[MW]	[Sec.]	[p.u.]	[kV]	[@ 0.5 Hz/s]	[@ 1.0 Hz/s]	[@ 0.5 Hz/s]	[@ 1.0 Hz/s]	[@ 1.5 Hz/s]	[@ 2.0Hz/s]
CCGT Single-shaft	400	5.5	1.9	20	Y	Y*	Y	Y*	Y*	N
CCGT Dual-Shaft	260	6	2.3	17	Y	Y*	Y	N	N	N
CCGT Dual-Shaft	140	9	2.1	17	Y	Y*	Y	N	N	N
Steam Thermal (Reheat)	300	5	1.7	17	Y	Y*	Y	Y*	Y*	N**
Steam Thermal (Once Through)	250	4.5	2.3	20	Y	Y*	Y*	Y*	N	N
Steam Thermal (Fluidized bed peat)	150	8	2.2	11	Y	Y*	Y*	N	N	N
OCGT	50	1.5	2.9	11	Y	Y*	Y*	Y*	Y*	Y*
Salient-pole Hydro	30	2.7	1.4	11	Y	Y	Y	Y	Y	Y

Definition of RoCoF is masking the real duration. Machine sees real time. More generators will not be compliant

## RoCoF values at various substations (EWIC problems)

Maximum RoCoF measurements for different time windows

Bus	T = 100 ms	T = 500 ms
AA	0.23	0.41
AD	1.07	0.41
CF	1.34	0.42
LOU	2.09	0.43
CKM	1.91	0.43
GI	1.56	0.42
BALLY	1.55	0.43
PB	2.71	0.53
<b>AVG</b>	<b>1.59</b>	<b>0.43</b>

Ardnacrusha (AA), Aghada (AD), Cathaleen's Fall (CF), Louth (LOU), Carrickmines (CKM), Great Island (GI), Ballylumford (BALLY) and Poolbeg (PB) (\*1)

**Problem: Generator sees actual values...**

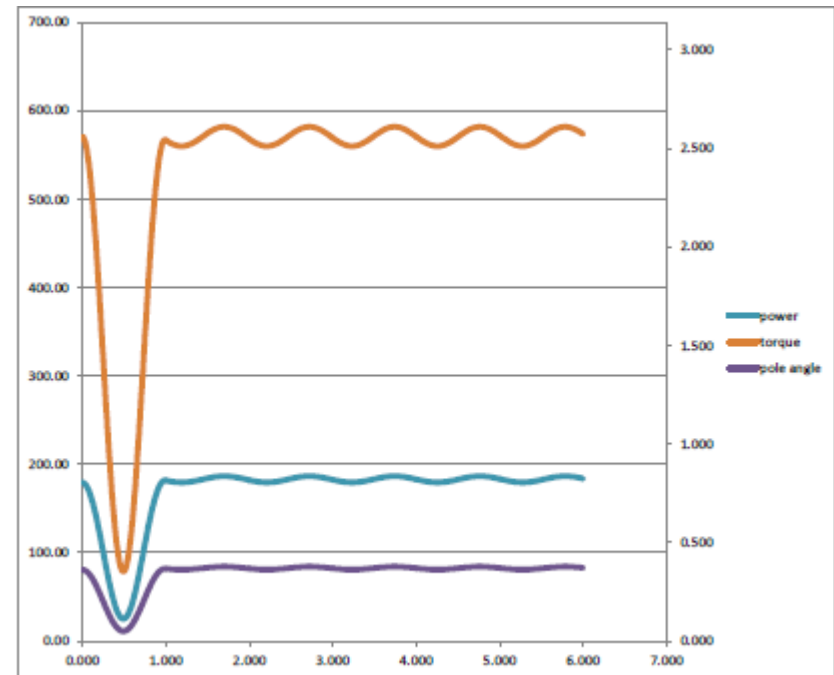
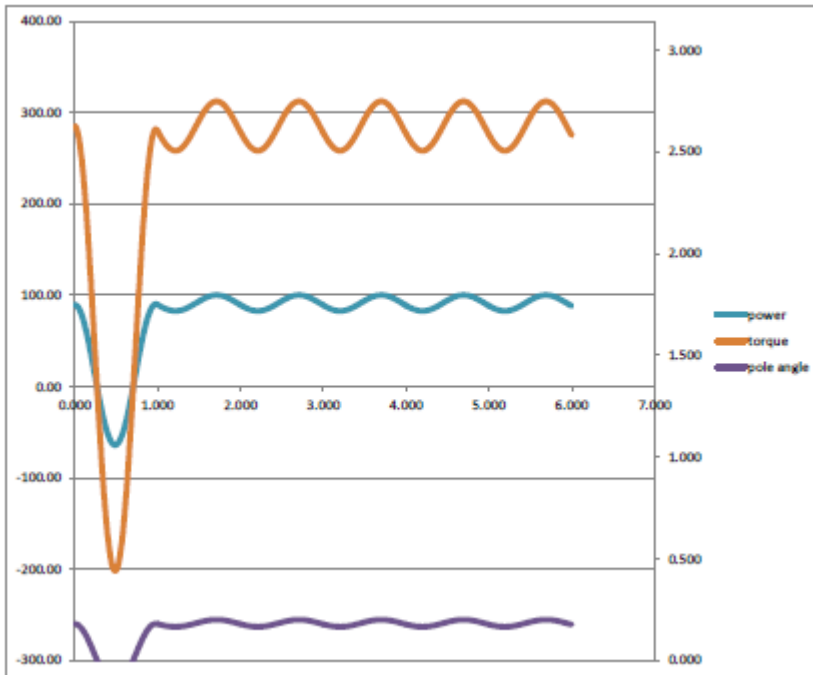
# 500ms vs 100ms Time Window

- Definition of RoCoF is questionable as the generator sees real time rather than windows
- Generators in Poolbeg will experience higher RoCoF values
- Compliance to the grid code can not be guaranteed without **exact** traces and an available model of the entire network or even a simplified model

## ESB Study, undertaken by DNV GL(former KEMA)



# Min Load Operation, Steam Turbine 25 and 50% Load, 50->51Hz, +1Hz/sec (KEMA Study commissioned by ESB)



Problems with Minimum Load to be anticipated (usual at night time)

\* Eirgrid-KEMA study did not analyse min load capability

# ESB Study, real values, example: Steam Turbine

## RoCoF Calculations For Synchronous Generator Regarding Torque And Stability

Generator 4, Poolbeg 1E, Steam Turbine connected at 2 HRSG's fed by Gas Turbines			ID	oocp	load	RoCoF 1	RoCoF 2	Stable	MaxTorque	Limit 1	Limit 2
Quantity/ Dimension	Value	SI Unit									
[Name/ Symbol]	[Number]	[Symbol]			[%]	[Hz/s]	[Hz/s]		[%]	[Hz]	[Hz]
Rated power	170	[MW]	A	1	25	-1.00	0.00	N**	118	49.0	50.0
Rated power factor	0.85		B	1	50	-1.00	0.00	N**	142	49.0	50.0
Rated voltage	15,750	[V]	C	1	75	-1.00	0.00	N**	151	49.0	50.0
Synchronous reactance	2.25	[p.u.]	D	1	100	-1.00	0.00	N	150	49.0	50.0
$f_s$	50	[Hz]	E	1	25	1.00	0.00	N**	29	51.0	51.0
p (pole pair number)	1		F	1	50	1.00	0.00	N**	59	51.0	51.0
H (stored energy constant)	10	[s]	G	1	75	1.00	0.00	N**	88	51.0	51.0
Rated power	200	[MVA]	H	1	100	1.00	0.00	N	118	51.0	51.0
Rated current	7,331	[A]	I	1	25	-0.50	0.00	N**	76	49.0	50.0
Rated torque	541	[kNm]	J	1	50	-0.50	0.00	Y	104	49.0	50.0
Reference reactance	1.240	[ $\Omega$ ]	K	1	75	-0.50	0.00	Y	132	49.0	50.0
Synchronous reactance	2.791	[ $\Omega$ ]	L	1	100	-0.50	0.00	Y	150	49.0	50.0
$\omega_s$	314.2	[rad/s]	M	1	25	0.50	0.00	N**	29	51.0	51.0
J	40528	[kgm <sup>2</sup> ]	N	1	50	0.50	0.00	Y	59	51.0	51.0
			O	1	75	0.50	0.00	Y	88	51.0	51.0
			P	1	100	0.50	0.00	Y	118	51.0	51.0

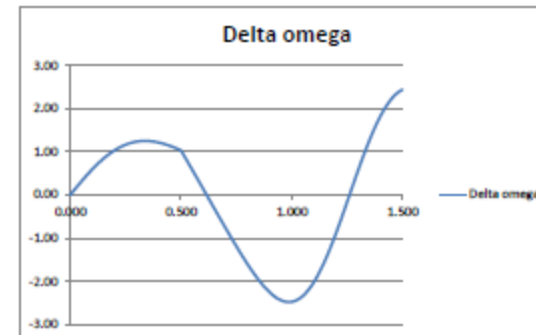
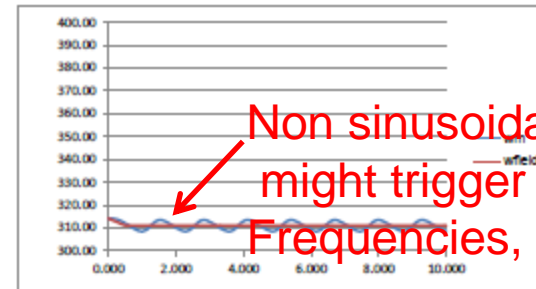
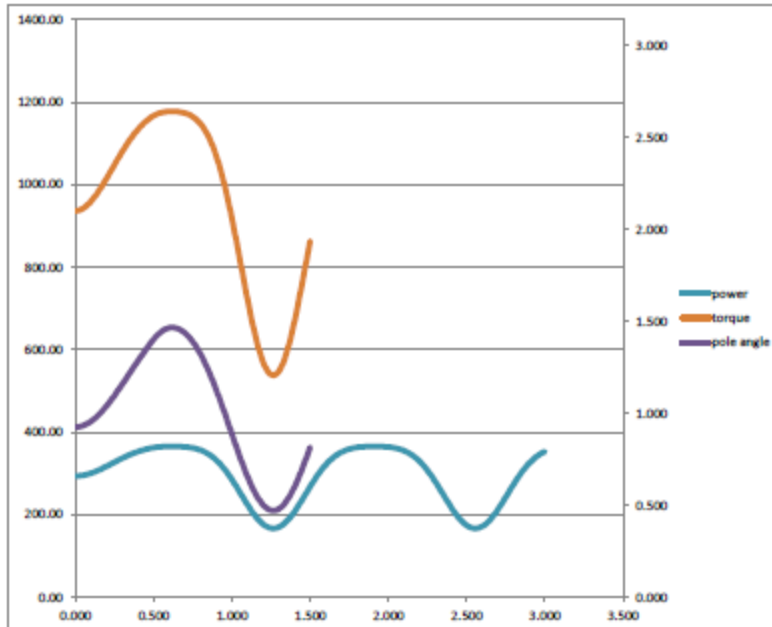
\*\*] Reverse Power and therefore assumed instability

Currently compliant with 0.5Hz/sec. With 1Hz/sec problems with compliance

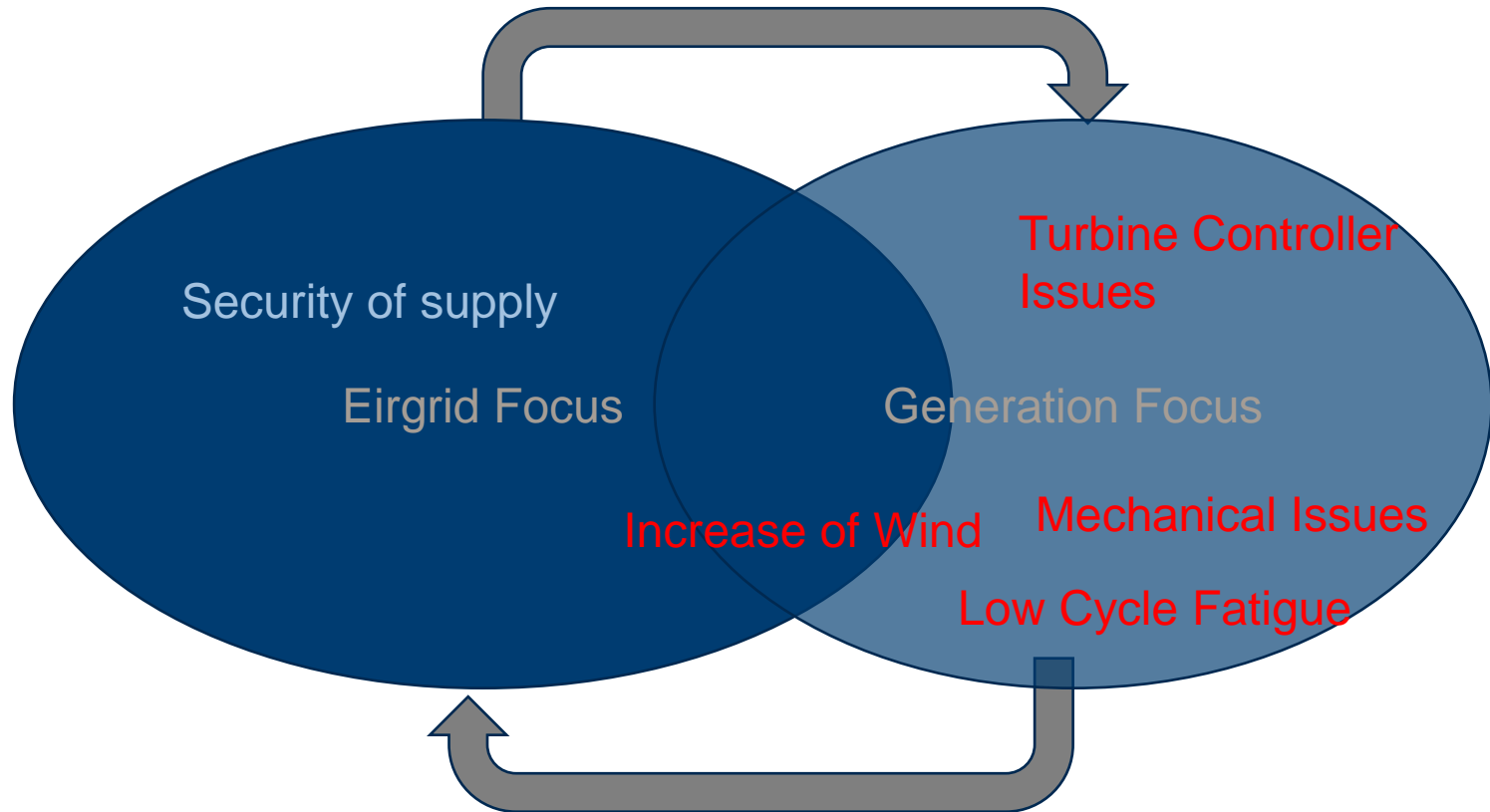
Calculation ID: K

Torque Calculation Synchronous Generator

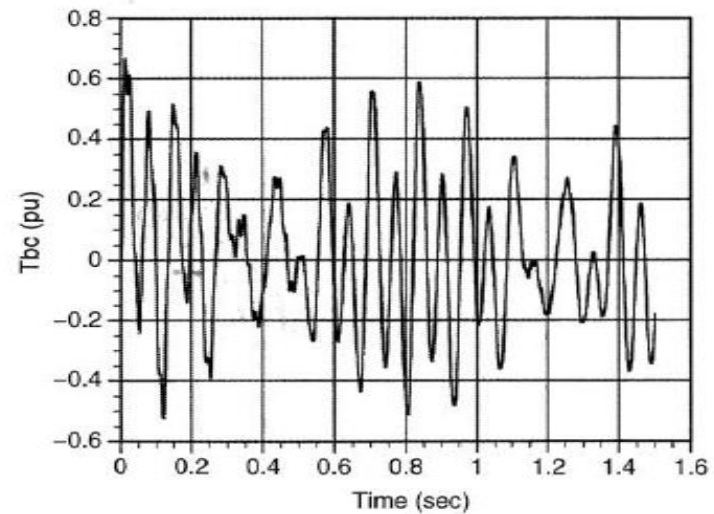
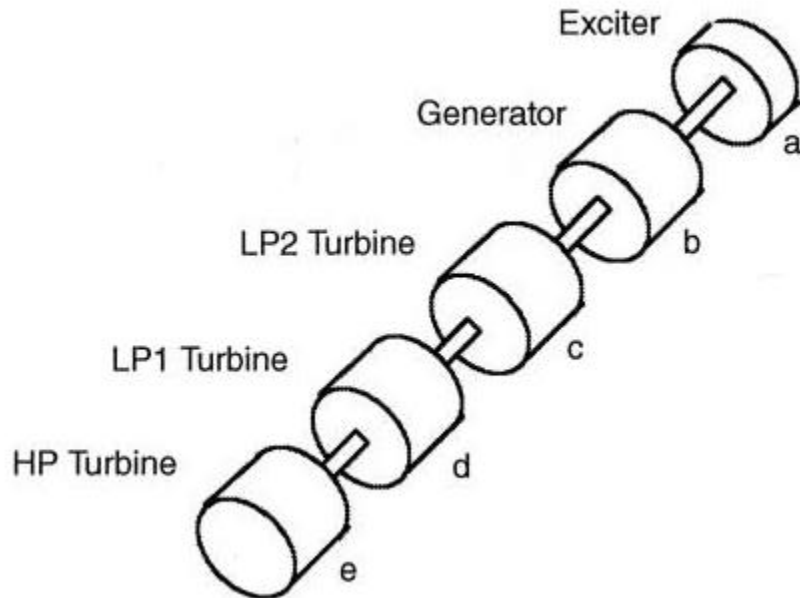
Quantity/ Dimension	Value SI Unit	Quantity/ Dimension	Value SI Unit	ID	oocp	load	RoCoF	Stable	MaxTorque	Limit
[Name/ Symbol]	[Number] [Symbol]	[Name/ Symbol]	[Number] [Symbol]		[-]	[%]	[Hz/s]	[Y]	[%]	[Hz/s]
Rated power	250 [MW]	Reference reactance	1.360 [ $\Omega$ ]	K	1	0	100	-1	Y	148
Rated power factor	0.83	Synchronous reactance	3.128 [ $\Omega$ ]		$\phi$		$\omega_{h, start}$			
Rated voltage	20000 [V]	$\omega_h$	314.2 [rad/s]		0	*	0.93			
Synchronous reactance	2.3 [p.u.]	$\delta$	0.93 [rad]	53.02						
$f_s$	50 [Hz]	$P_{max}$	294.1 [MW]							
p (pole pair number)	1	Cpower	368.2							
H (stored energy constant)	4.3 [s]	$T_{max}$	936 [kNm]							
Rated power	294 [MVA]	J	26820 [kgm <sup>2</sup> ]							
Rated current	8490 [A]	Max. torque (500 ms)	147 [%]							
Rated torque	796 [kNm]	Max. torque (1 s)	148 [%]							



- **Minimum Load Problematic**
- **Compliance of existing machines especially with high inertia at 1Hz/s**
- **Further investigations required due to problems with non-sinusoidal oscillations**



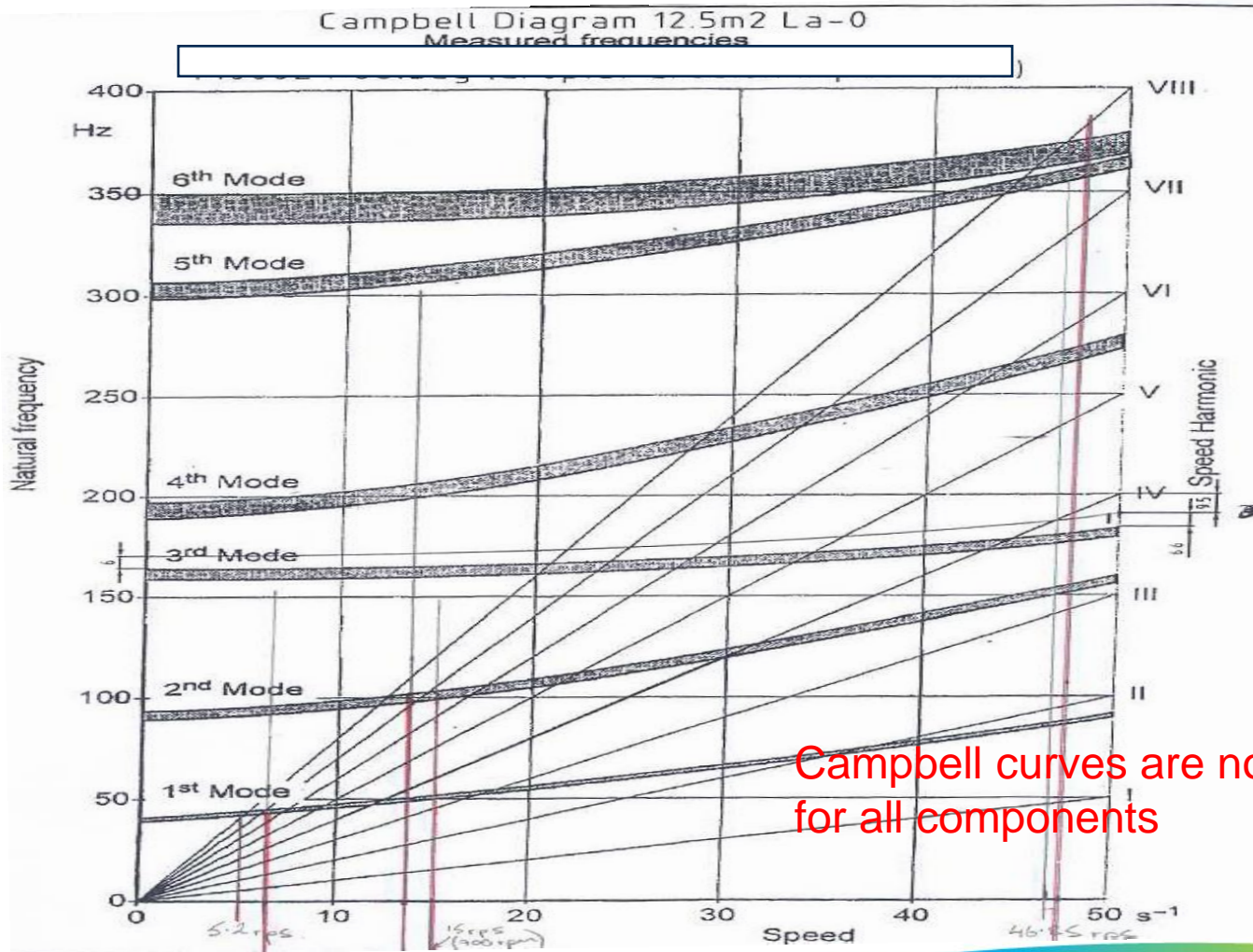
## Analysis for impact at mechanical components



Shaft section b-c torque for three-phase fault.

Higher RoCoF values might trigger Eigen-Frequencies

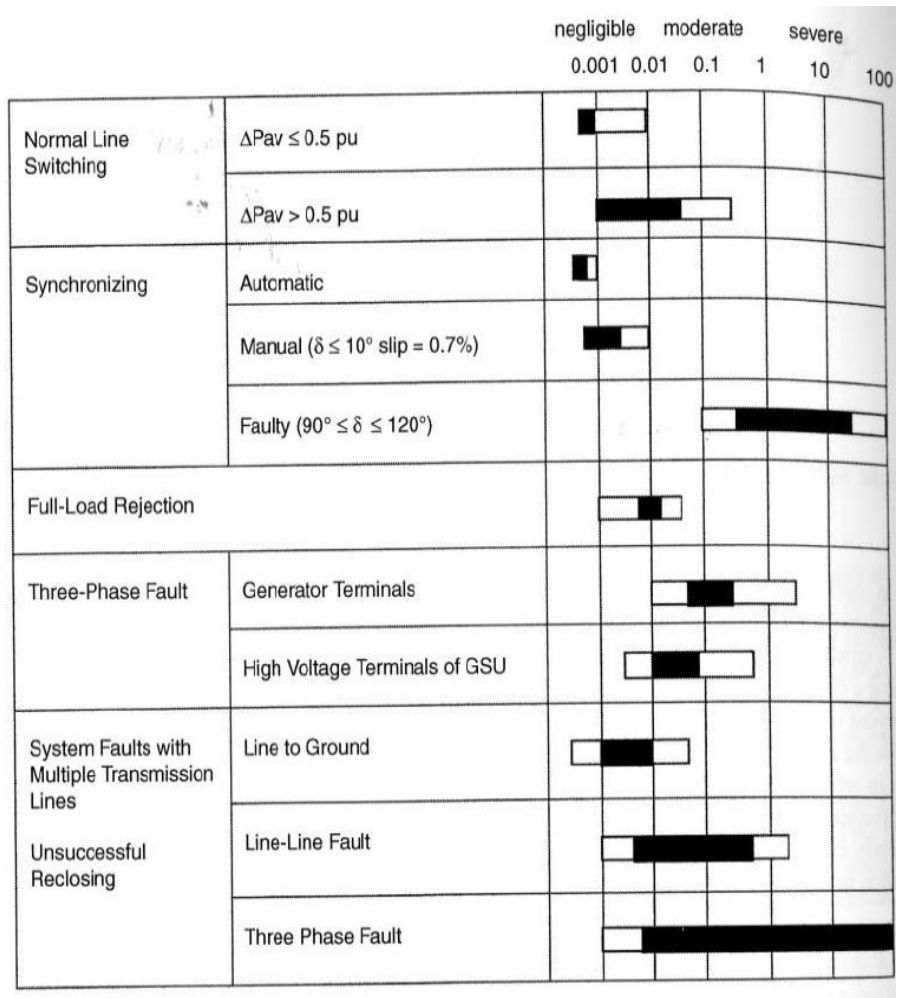
# Natural Frequencies of Components, Example LP-Blades row 0 (Last stage blades)



Campbell curves are not available for all components



# Impact on lifetime



Life time and maintenance analysis to be undertaken



Further analysis of RoCoF events is required:

.....Therefore the increase of 153 % in torque of the nominal value will not cause immediate failure of the synchronous machines currently compliant with the Ireland and Northern Ireland grid code. Considerations however may **need to be made regarding lifetime reduction/ maintenance intervals. Allowing multiple RoCoF events each year could effect lifetime.**

RoCoF, An independent analysis on the ability of Generators to ride through Rate of Change of Frequency values up to 2Hz/s.  
(8.2.2013 KEMA)

- Dynamic analysis with accurate models is required.  
Digsilent models to be developed
- Information collection, especially mechanical components
- Life time analysis and crack and failure mechanisms need to be investigated

1. **Stability - > Mechanical Issues**
2. **Definition of RoCoF (500ms) – > Suitable Trace required to check compliance**
3. **Operation at leading power factors - > Operational Issues**
4. **Issues at Min Gen - > Capability unavailable when most required i.e. at night**

1. **“DNV\_KEMA\_Report\_Rocof\_20130208v3.pdf”, commissioned by Eirgrid**
2. **“Summary of Studies on Rate of Change of Frequency events on the All-Island System”, August 2012, Salim Temtem & Karen Creighton (Eirgrid)**
3. **“Protective Relaying for Generation Systems”, Donald Reimert**

- Major doubt over feasibility of 1Hz/s
  - Mechanical issue
  - Operational issues
  - Min Gen
- Data Requirements
- Eirgrid unsuitable for PM Role
- Unrealistic timelines for OEM's to meet
- Cost Recovery